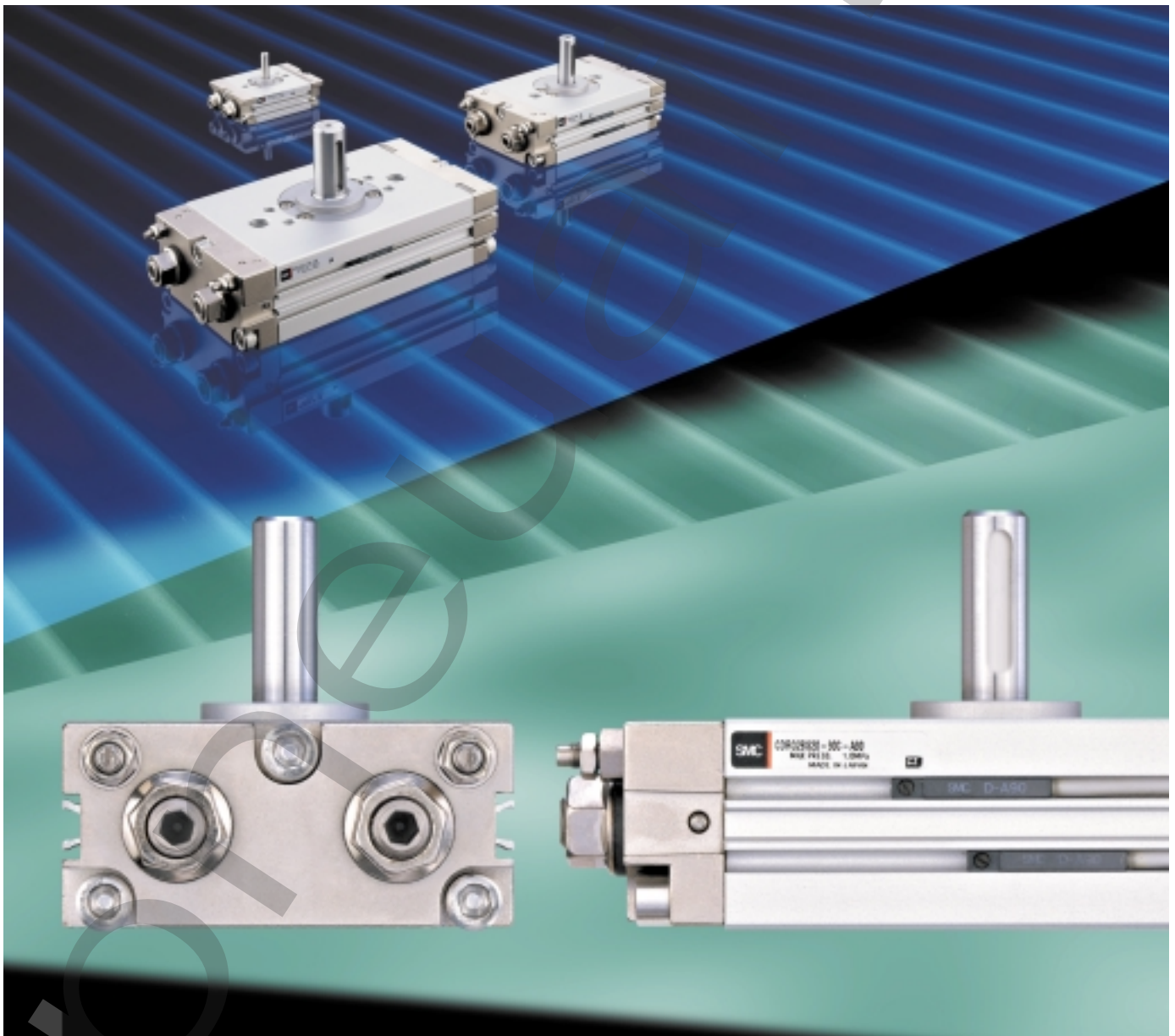


Compact Rotary Actuator
Rack-and-Pinion Type/Sizes: 10, 15, 20, 30, 40

Series **CRQ2**



Compact Rotary Actuator
Rack-and-Pinion Type/Sizes: 10, 15, 20, 30, 40

Series CRQ2

Piping can be installed from one end

Body can be used as a flange

Uses internal cushioning

10, 15 : Rubber bumper
20, 30, 40: Air cushion

Compact design saves mounting space

10: 17mm
15: 20mm
20: 29mm
30: 33mm
40: 37mm



2 auto switches can be mounted on same side (both sides)

Miniature auto switches do not protrude from the body when installed and require no extra space.

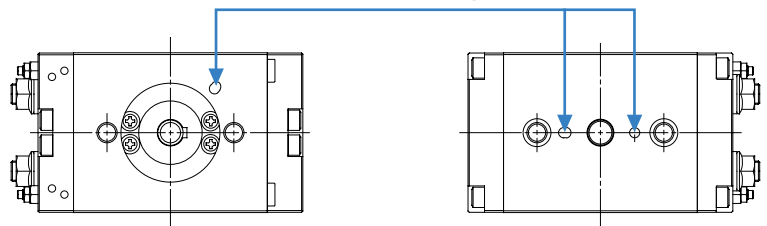
Angle adjustment bolts are standard

Use of double piston eliminates backlash

Easy alignment when mounting body

Body positioning pin holes

Single and double shaft types available in all sizes



Variations

	10	15	20	30	40
Rotation	80° to 100° 170° to 190°				
Auto switches	●	●	●	●	●
Air cushion			●	●	●
Rubber bumper	●	●			
Single shaft type (S)	●	●	●	●	●
Double shaft type (W)	●	●	●	●	●

Compact Rotary Actuator Rack-and-Pinion Type

Series CRQ2

How to Order

Standard type

CRQ2B S 20-90

Shaft type	
Single shaft	S
Double shaft	W
Size	
10	
15	
20	
30	
40	
Rotation	
90	80° to 100°
180	170° to 190°
Air cushion	
Sizes	Air cushion
10, 15	Without Nil
20, 30, 40	Without Nil
	With C

With auto switch

CDRQ2B S 20-90 A90 S

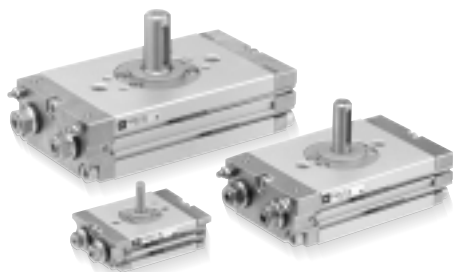
Built-in magnet	
Shaft type	
Single shaft	S
Double shaft	W
Size	
10	
15	
20	
30	
40	
Rotation	
90	80° to 100°
180	170° to 190°
Air cushion	
Sizes	Air cushion
10, 15	Without Nil
20, 30, 40	Without Nil
	With C
Auto switch model	
Nil	Without auto switch (built-in magnet)
* Select applicable auto switch models from the table below.	
Number of auto switches	
Nil	2 pcs.
S	1 pc.

Applicable auto switches

Type	Special function	Electrical entry	Indicator light	Wiring (output)	Load voltage		Auto switch part no.		Lead wire length (m)*			Applicable loads				
					DC	AC	Electrical entry direction	0.5 (Nil)	3 (L)	5 (Z)	IC circuit	Relay, PLC				
						Perpendicular	In-line									
Reed switch	—	Grommet	Yes	3 wire (NPN equiv.)	—	5V	—	A96V	A96	●	—	—	—	—		
								A96VL	A96L	—	●	—				
				A93V	A93	●	—	—	—	Relay, PLC						
				A93VL	A93L	—	●	—								
Solid state switch	Diagnostic indication (2 color indicator)	Grommet	Yes	3 wire (NPN)	24V	5V, 12V	—	A90V	A90	●	—	—	—	Relay, PLC		
								A90VL	A90L	—	●	—				
				3 wire (PNP)	—	—	—	—	—	F9NV	F9N	●	—	—	—	Relay, PLC
										F9NVL	F9NL	—	●	—		
				2 wire	—	—	—	—	—	F9NVZ	F9NZ	—	—	○	—	Relay, PLC
										F9PV	F9P	●	●	—		
				3 wire (NPN)	—	—	—	—	—	F9PVL	F9PL	—	●	—	—	Relay, PLC
										F9PVZ	F9PZ	—	—	○		
				2 wire	—	—	—	—	—	F9BV	F9B	●	—	—	—	Relay, PLC
										F9BVL	F9BL	—	●	—		
				3 wire (NPN)	—	—	—	—	—	F9BVZ	F9BZ	—	—	○	—	Relay, PLC
										F9NWV	F9NW	●	—	—		
				3 wire (PNP)	—	—	—	—	—	F9NWVL	F9NWL	—	●	—	—	Relay, PLC
										F9NWVZ	F9NWZ	—	—	○		
				2 wire	—	—	—	—	—	F9PWV	F9PW	●	—	—	—	Relay, PLC
										F9PWVL	F9PWL	—	●	—		
3 wire (NPN)	—	—	—	—	—	F9PWVZ	F9PWZ	—	—	○	—	Relay, PLC				
						F9BWV	F9BW	●	—	—						
2 wire	—	—	—	—	—	F9BWVL	F9BWL	—	●	—	—	Relay, PLC				
						F9BWVZ	F9BWZ	—	—	○						

*Lead wire length symbols 0.5m ... Nil (Example) F9B 3m L (Example) F9BL 5m Z (Example) F9BZ * Solid state auto switches marked with a ○ are produced upon receipt of order.

Series CRQ2



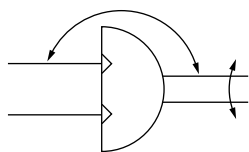
Specifications

Size	10	15	20	30	40
Fluid	Air (unlubricated)				
Maximum operating pressure	0.7MPa		1MPa		
Minimum operating pressure	0.15MPa		0.1MPa		
Ambient and fluid temperature	0 to 60°C (with no freezing)				
Cushion	Rubber bumper		None, Air cushion		
Angle adjustment	± 5°				
Rotation	80° to 100°, 170° to 190°				
Port size	M5 x 0.8		Rc1/8		
Mounting brackets	Basic type				
Output Nm*	0.3	0.75	1.8	3.1	5.3

*) Indicates output with operating pressure at 0.5MPa. Refer to Page 14 for details.

Allowable Kinetic Energy and Rotation Time Adjustment Range

JIS symbol



Size	Allowable kinetic energy				Cushion angle	Stable operational rotation time adjustment range
	Allowable kinetic energy (J)			Rotation time (s/90°)		
	Without cushion	Rubber bumper	With air cushion *			
10	—	0.25 x 10 ⁻³	—	—	0.2 to 0.7	
15	—	0.39 x 10 ⁻³	—	—	0.2 to 0.7	
20	0.025	—	0.12	40°	0.2 to 1	
30	0.048	—	0.25	40°	0.2 to 1	
40	0.081	—	0.40	40°	0.2 to 1	

*) Allowable kinetic energy with cushion
Maximum energy absorption with optimal adjustment of cushion needle

Weight Table

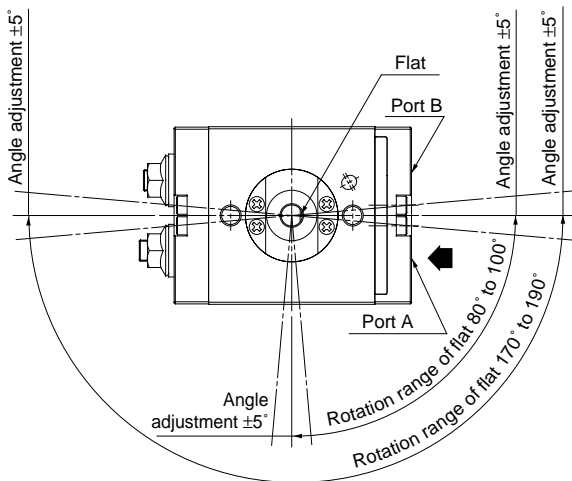
Size	Standard weight* (g)	
	90°	180°
10	120	150
15	220	270
20	600	700
30	900	1100
40	1400	1600

*) Value excluding the weight of auto switches.

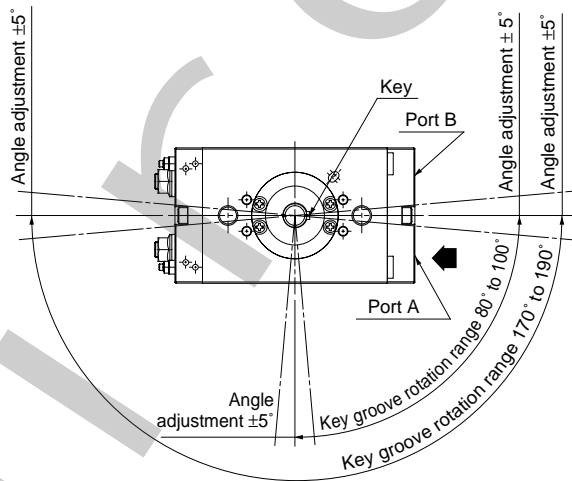
Rotation Range

When pressure is applied to the port on the side with the arrow, the shaft rotates clockwise.

Sizes 10, 15



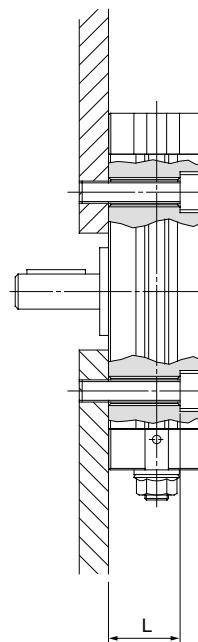
Sizes 20, 30, 40



Using the Body as a Flange

The body's L dimensions are shown in the drawing on the right.

When JIS standard hexagon socket head cap screws are used, the actuator grooves should be used to contain the heads of the screws.

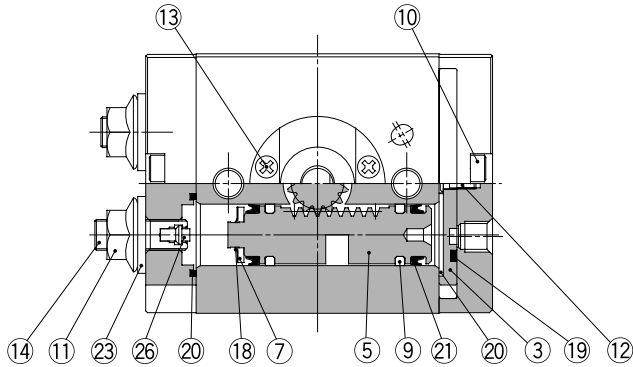


Size	L	Screw
10	13	M4
15	16	M4
20	22.5	M6
30	24.5	M8
40	28.5	M8

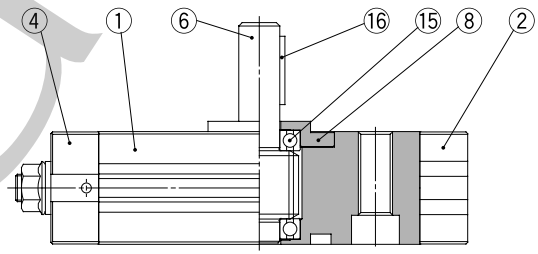
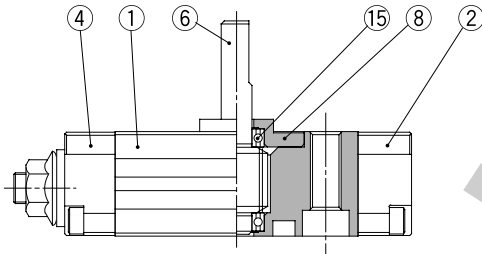
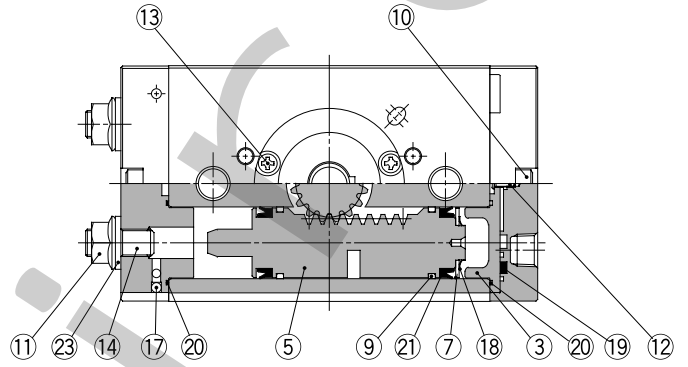
Series CRQ2

Construction

Standard type
Sizes 10, 15



Standard type
Sizes 20, 30, 40



Parts list

No.	Description	Material	Note
1	Body	Aluminum alloy	Clear hard anodized
2	Cover	Aluminum alloy	Electroless nickel plated
3	Plate	Aluminum alloy	
4	End cover	Aluminum alloy	Electroless nickel plated
5	Piston	Stainless steel	
6	Shaft	Stainless steel	Sizes: 10, 15
		Chromium molybdenum steel	Sizes: 20, 30, 40
7	Seal retainer	Aluminum alloy	Chromated
8	Bearing retainer	Aluminum alloy	Clear hard anodized
9	Wear ring	Resin	
10	Hexagon socket head cap screw	Stainless steel	
11	Hexagon nut with flange	Steel wire	Electroless nickel plated
12	Round head No. 0 Phillips screw	Steel wire	Zinc chromated
13	Round head No. 0 Phillips screw	Steel wire	10, 15 nickel plated
	Round head Phillips screw		20, 30, 40 nickel plated

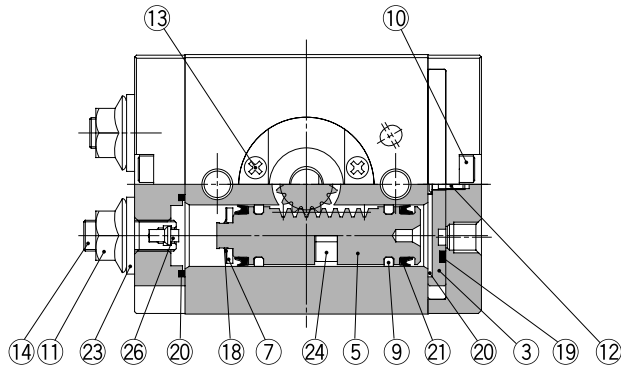
Parts list

No.	Description	Material	Note
14	Hexagon socket head set screw	Chromium molybdenum steel	Electroless nickel plated
15	Bearing	Bearing steel	
16	Parallel key	Carbon steel	20, 30, 40
17	Steel balls	Stainless steel	20, 30, 40
18	C S type snap ring	Stainless steel	
19	Seal	NBR	
20	Gasket		
21	Piston seal		
22	Cushion seal		20, 30, 40 with cushion
23	Seal washer		
24	Magnet	Magnetic material	With auto switch
25	Cushion valve assembly		20, 30, 40 with cushion
26	Cushion pad	Elastic material	10, 15

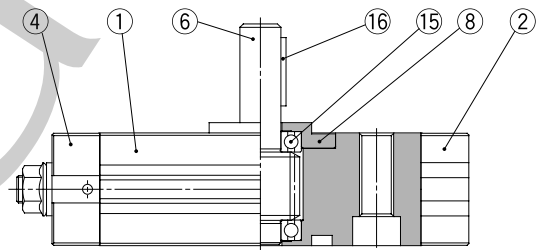
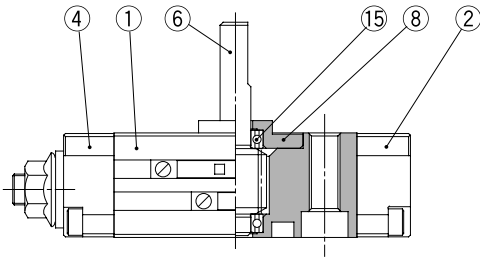
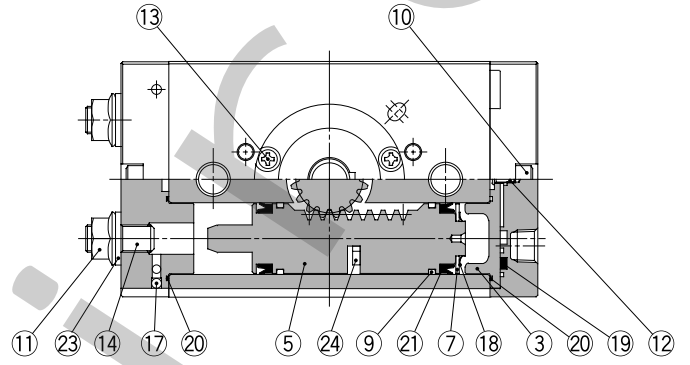
Replacement parts

Description	Kit number					Contents
	10	15	20	30	40	
Seal kit	P473010-1	P473020-1	P473030-1	P473040-1	P473050-1	19, 20, 21, 23

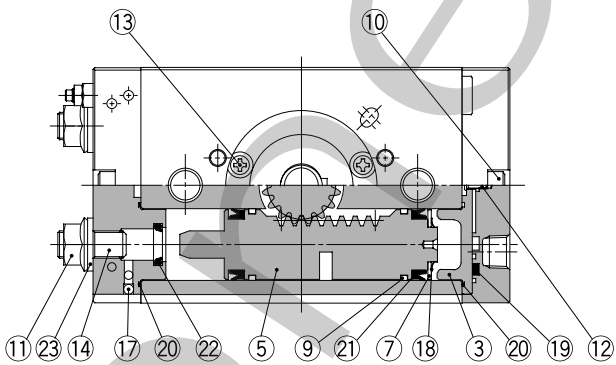
With auto switch
Sizes 10, 15



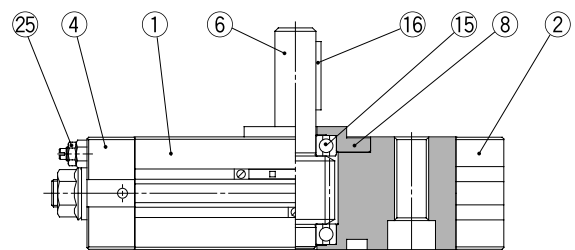
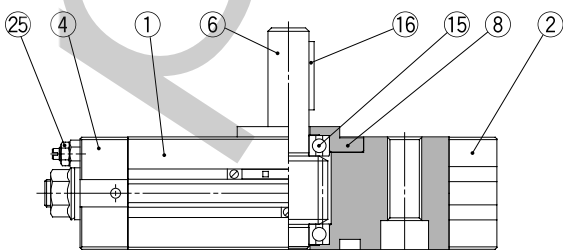
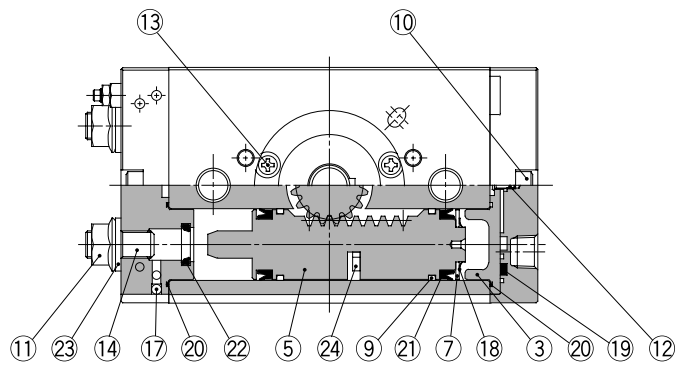
With auto switch
Sizes 20, 30, 40



With cushion
Sizes 20, 30, 40



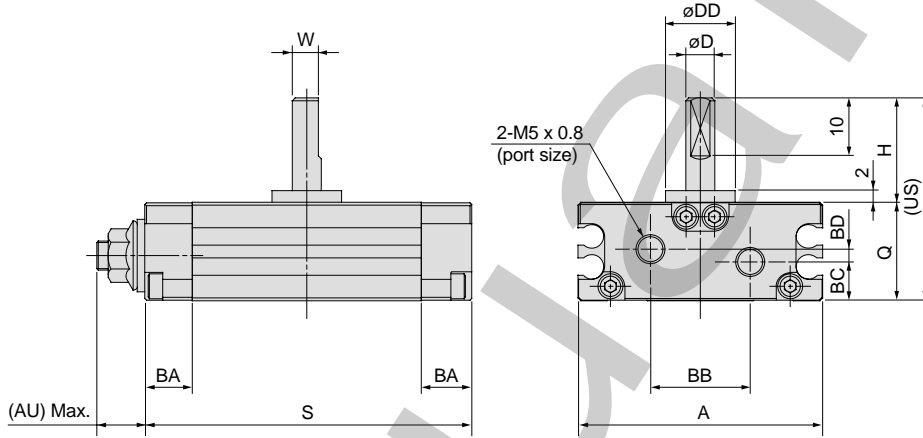
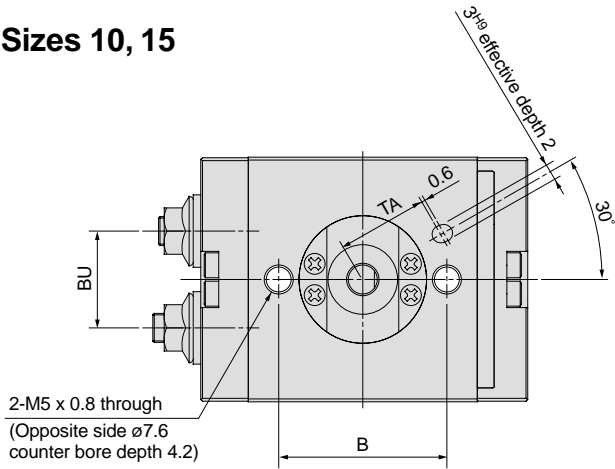
With auto switch and cushion
Sizes 20, 30, 40



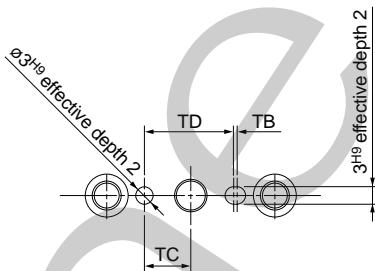
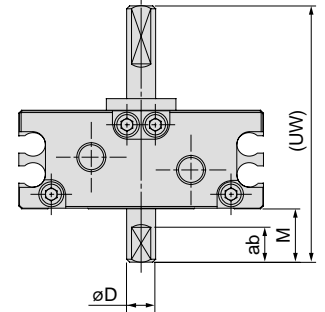
Series CRQ2

Dimensions

Sizes 10, 15



With double shaft



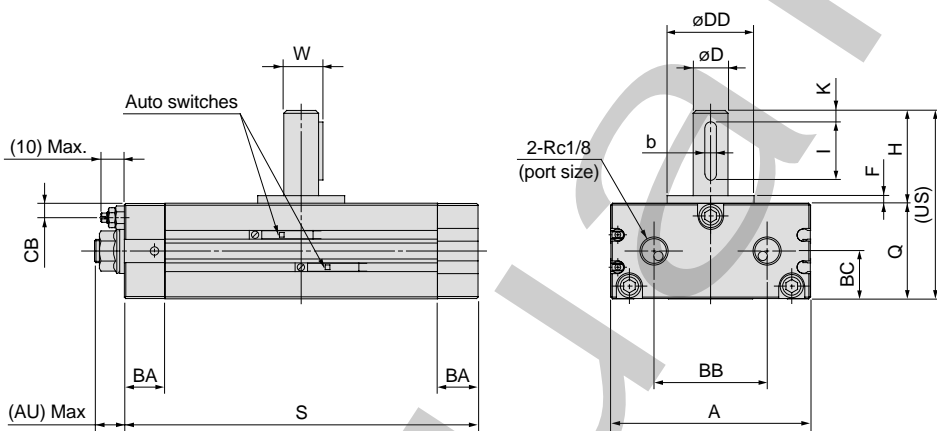
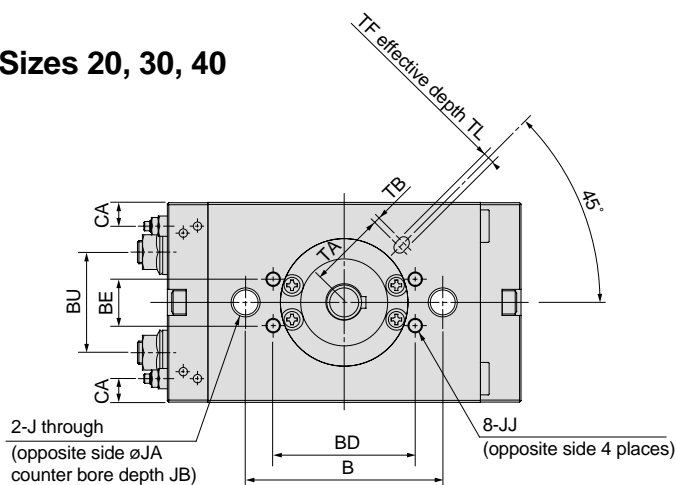
Size	Rotation	A	AU*	B	BA	BB	BC	BD	BU	D (g6)	DD (h9)	H
10	90°, 180°	42	(8.5)	29	8.5	17	6.7	2.2	16.7	5	12	18
15	90°, 180°	53	(9.5)	31	9	26.4	10.6	-	23.1	6	14	20

Size	Rotation	W	Q	S	US	UW	ab	M	TA	TC	TD
10	90°	4.5	17	56	35	44	6	9	15.5	8	15.4
	180°			69							
15	90°	5.5	20	65	40	50	7	10	16	9	17.6
	180°			82							

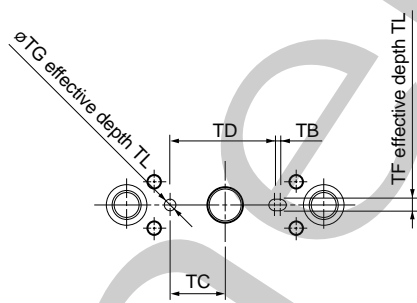
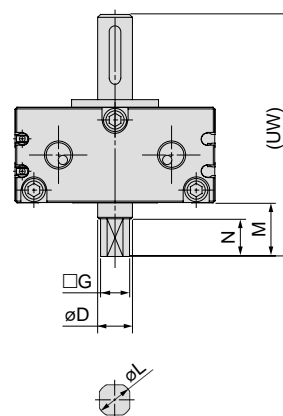
* Dimension AU does not indicate the dimension when shipped because of the adjustment section.

S: Upper space 90°, Lower space 180°

Sizes 20, 30, 40



With double shaft



Size	Rotation	A	AU*	B	BA	BB	BC	BD	BE	BU	CA	CB	D (g6)	DD (h9)	F	H	J	JA	JB
20	90°, 180°	63	(11)	50	14	34	14.5	—	—	30.4	7	4.7	10	25	2.5	30	M8 x 1.25	11	6.5
30	90°, 180°	69	(11)	68	14	39	16.5	49	16	34.7	8.1	4.9	12	30	3	32	M10 x 1.5	14	8.5
40	90°, 180°	78	(13)	76	16	47	18.5	55	16	40.4	8.3	5.2	15	32	3	36	M10 x 1.5	14	8.6

Size	Rotation	JJ	K	Q	S	W	Key dimensions		US	TA	TB	TC	TD	TF (H9)	TG (H9)	TL	UW	G	M	N	L
							b	l													
20	90°	—	3	29	104	11.5	4 ⁰ _{-0.03}	20	59	24.5	1	13.5	27	4	4	2.5	74	8	15	11	9.6
	180°				130																
30	90°	M5 x 0.8 depth 6	4	33	122	13.5	4 ⁰ _{-0.03}	20	65	27	2	19	36	4	4	2.5	83	10	18	13	11.4
	180°				153																
40	90°	M6 x 1 depth 7	5	37	139	17	5 ⁰ _{-0.03}	25	73	32.5	2	20	39.5	5	5	3.5	93	11	20	15	14
	180°				177																

* Dimension AU does not indicate the dimension when shipped because of the adjustment section.

S: Upper space 90°, Lower space 180°

Series CRQ2 Auto Switch Specifications

Reed Switches



Auto switch part no.	Load voltage	Maximum load current or load current range	Internal voltage drop	Indicator light (lights when ON)	Applications
D-A90 D-A90V	AC 24V or less	50mA	0	None	Relay, PLC, IC circuit
	DC 48V or less	40mA			
	DC 100V or less	20mA			
D-A93 D-A93V	24VDC	5 to 40mA	2.6V or less	●	Relay, PLC
	100VAC	5 to 20mA			
D-A96 D-A96V	4 to 8VDC	20mA	0.8V or less	●	IC circuit

- Lead wires — D-A90□, A93□: Oil resistant heavy duty vinyl cord ø2.7 0.18mm² x 2 wire (Brown, Blue [Red, Black]) 0.5m
D-A96□: Oil resistant heavy duty vinyl cord ø2.7 0.15mm² x 3 wire (Brown, Black, Blue [Red, White, Black]) 0.5m
- Insulation resistance — 50MΩ or more at 500VDC (between lead wire and case)
- Withstand voltage — 1000VAC for 1 min. (between lead wire and case) • Operation time — 1.2ms
- Ambient temperature — 10 to 60°C • Impact resistance — 300m/s² {30.6G} • Leakage current — 0
- Enclosure — IEC529 standard IP67 (JIS0920) watertight
- For a lead wire length of 3m, "L" is added to the end of the part number. Example) D-A90L

Solid State Switches

Auto switch part no.	Output type	Power supply voltage	Current consumption	Load voltage	Max. load current or load current range	Internal voltage drop	Leakage current	Indicator light	Applications
D-F9N D-F9NV	NPN type	24VDC (10 to 28VDC)	8mA or less	28VDC or less	50mA or less	0.4V or less	10μA or less at 24VDC	Lights when ON	Relay, PLC
D-F9NW D-F9NWW			12mA or less					2 color indicator	
D-F9P D-F9PV	PNP type		10mA or less	—				1.5V or less	
D-F9PW D-F9PWW		2 color indicator							
D-F9B D-F9BV	—	—	—	24VDC (10 to 28VDC)	5 to 30mA	4.5V or less	1mA or less at 24VDC	Lights when ON	24VDC Relay, PLC
D-F9BW D-F9BWW								2 color indicator	

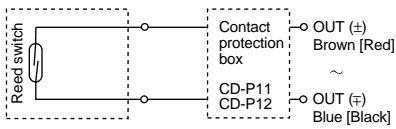
- Lead wires — Oil resistant heavy duty vinyl cord ø2.7, 0.15mm² x 3 wire (Brown, Black, Blue [Red, White, Black]) 0.5m, 0.18mm² x 2 wire (Brown, Blue [Red, Black]) 0.5m
- Insulation resistance — 50MΩ or more at 500VDC (between lead wire and case)
- Withstand voltage — 1000VAC for 1 min. (between lead wire and case)
- Ambient temperature — 10 to 60°C • Operation time — 1ms or less
- Impact resistance — 1000m/s² {102G}
- Enclosure — IEC529 standard IP65 (JIS0920) splash proof
- For a lead wire length of 3m, "L" is added to the end of the part number. Example) D-F90NL

Auto Switch Internal Circuits

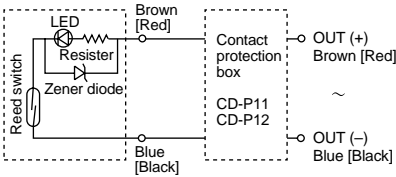
Lead wire colors inside [] are those prior to conformity with IEC standards.

Reed switches

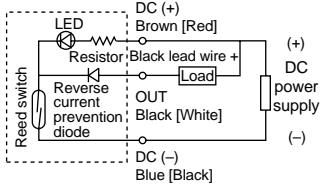
D-A90 (V)



D-A93 (V)

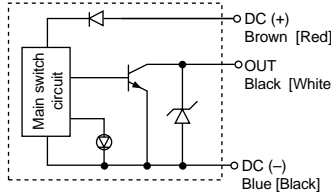


D-A96 (V)

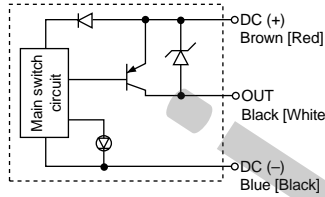


Solid state switches

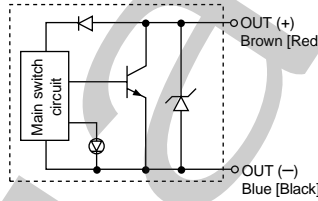
D-F9N (V)



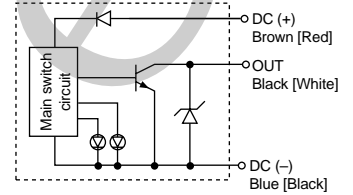
D-F9P (V)



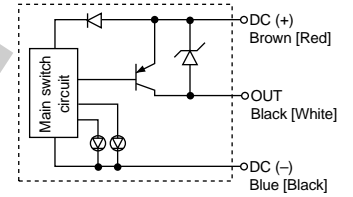
D-F9B (V)



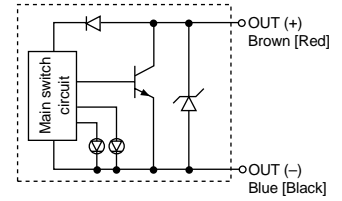
D-F9NW (V)



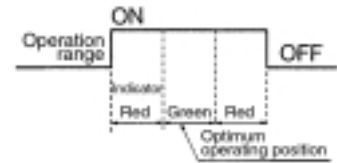
D-F9PW (V)



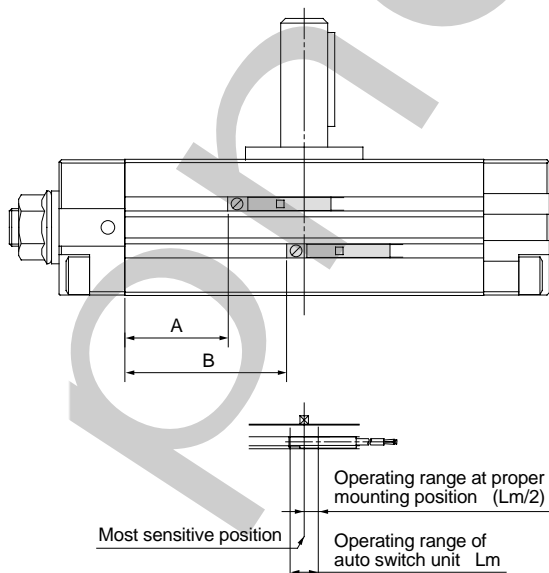
D-F9BW (V)



Indicator light/Display method



Proper Auto Switch Mounting Positions



Size	Rotation angle	Reed switches				Solid state switches			
		A	B	Operation range ϑ_m	Switch actuation range	A	B	Operation range ϑ_m	Switch actuation range
10	90°	6.5	13	63°	12°	10.5	17	75°	3°
	180°	9.5	22.5			13.5	26.5		
15	90°	9.5	18	52°	9°	13.5	22	69°	3°
	180°	13.5	30.5			17.5	34.5		
20	90°	22	34.5	41°	9°	26	38.5	56°	4°
	180°	28	53.5			32	57.5		
30	90°	29	45	32°	7°	33	49	43°	3°
	180°	37	68			41	72		
40	90°	34	53	24°	5°	38	57	36°	4°
	180°	43.5	81.5			47.5	85.5		

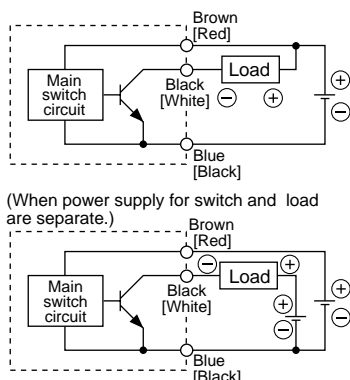
Operation range ϑ_m : The value of the auto switch operating range Lm converted to the shaft rotation angle

Switch actuation range: The value of the auto switch hysteresis converted to an angle

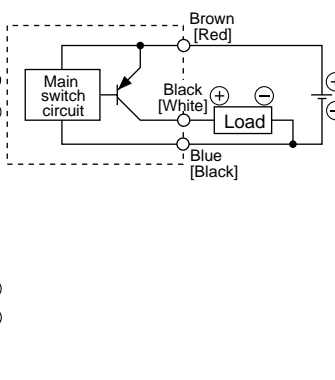
Series CRQ2 Auto Switch Connections and Examples

Basic Wiring

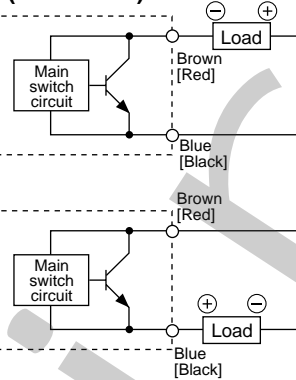
Solid state 3 wire, NPN



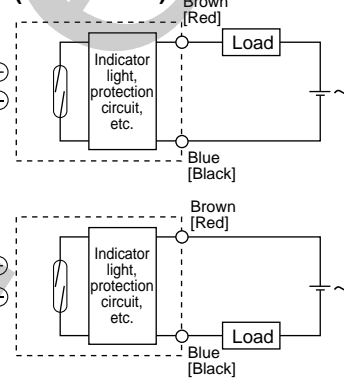
Solid state 3 wire, PNP



2 wire (Solid state)

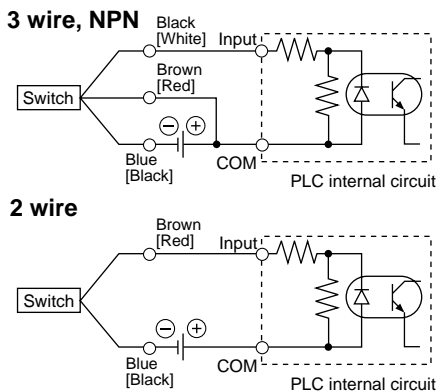


2 wire (Reed switch)

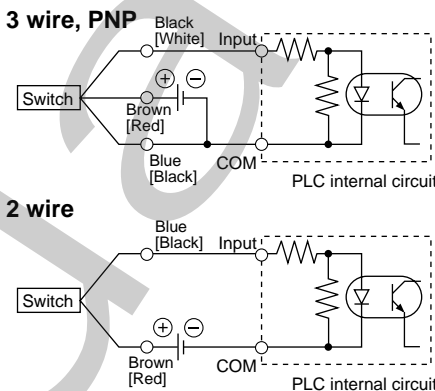


Examples of Connection to PLC

Sink input specifications



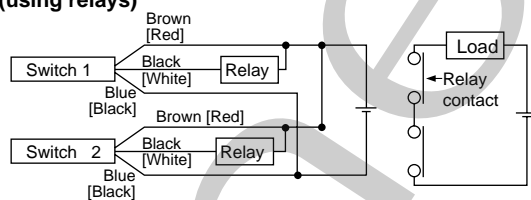
Source input specifications



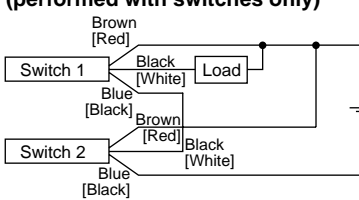
Connect according to the applicable PLC input specifications, as the connection method will vary depending on the PLC input specifications.

Connection Examples for AND (Series) and OR (Parallel)

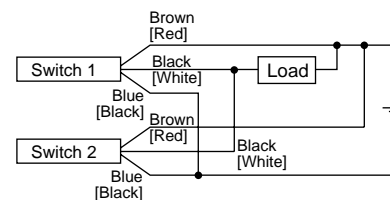
3 wire AND connection for NPN output (using relays)



AND connection for NPN output (performed with switches only)

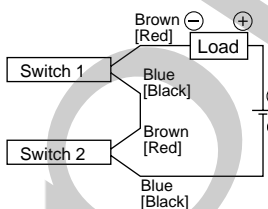


OR connection for NPN output



The indicator lights will light up when both switches are turned ON.

2 wire with 2 switch AND connection

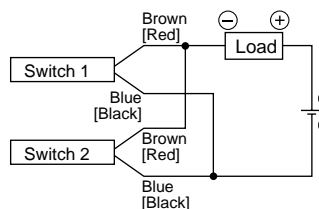


When two switches are connected in series, a load may malfunction because the load voltage will decline when in the ON state. The indicator lights will light up if both of the switches are in the ON state.

$$\begin{aligned} \text{Load voltage at ON} &= \text{Power supply voltage} - \text{Residual voltage} \times 2 \text{ pcs.} \\ &= 24\text{V} - 4\text{V} \times 2 \text{ pcs.} \\ &= 16\text{V} \end{aligned}$$

Example: Power supply is 24VDC
Voltage decline in switch is 4V

2 wire with 2 switch OR connection



(Solid state)
When two switches are connected in parallel, malfunction may occur because the load voltage will increase when in the OFF state.

(Reed switch)
Because there is no current leakage, the load voltage will not increase when turned OFF. However, depending on the number of switches in the ON state, the indicator lights may sometimes get dark or not light up, because of dispersion and reduction of the current flowing to the switches.

$$\begin{aligned} \text{Load voltage at OFF} &= \text{Leakage current} \times 2 \text{ pcs.} \times \text{Load impedance} \\ &= 1\text{mA} \times 2 \text{ pcs.} \times 3\text{k}\Omega \\ &= 6\text{V} \end{aligned}$$

Example: Load impedance is 3kΩ
Leakage current from switch is 1mA



Series CRQ2 Model Selection

Series CRQ2 Technical Information

Refer to pages 14 through 18 for detailed technical information other than series CRQ2 model selection procedures.

[Data 1] Effective torque [Data 2] Moment of Inertia [Data 3] Air consumption

Step

1

Select the actuator torque.

1. Find the required turning torque for the intended objective.

Work objective	Type of load	Required torque formula N·m ³
Static operation	Static load	T _s
Dynamic ^{*1} operation	Resistance load	(3 to 5) · T _f
	Inertial load ^{*2}	S · T _a or more

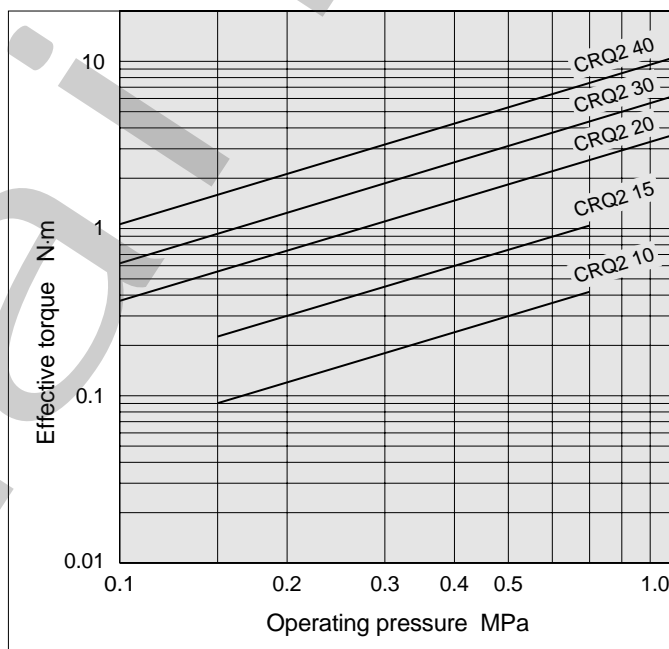
*1. In the case of dynamic operation, there may be a combination of resistance and inertial loads.

*2. Since it is also necessary to examine inertial load in selection step [2] in calculating the kinetic energy of the work piece, make the selections together.

*3. Refer to load types below for details regarding the terms T_s, T_f, S and T_a in the table.

2. Determine the operating pressure

3. Determine the proper size from the effective torque table.



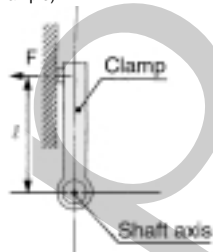
Load Types

● Static load: T_s

The load represented by the clamp which requires pressing force only

(During the course of examination, if it is decided to consider the mass of the clamp itself in the drawing below, it should be regarded as an inertial load.)

(Example)



F: Pressing force (N)
Static torque calculation
 $T_s = F \times l$ (N·m)

● Resistance load: T_f

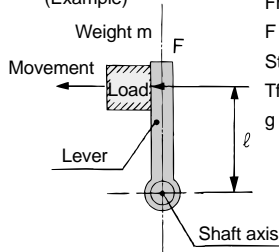
The load that is affected by external forces such as friction or gravity

Since the object is to move the load, and speed adjustment is necessary, allow an extra margin of 3 to 5 times in the effective torque.

* Actuator effective torque $\geq (3 \text{ to } 5) T_f$

(During the course of examination, if it is decided to consider the mass of the lever itself in the drawing below, it should be regarded as an inertial load.)

(Example)



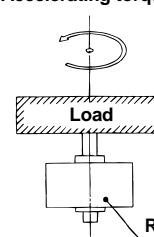
Friction coefficient μ
 $F = \mu mg$
Static torque calculation
 $T_f = F \times l$ (N·m)
 $g = 9.8 \text{ m/s}^2$

● Inertial load: T_a

The load which must be rotated by the actuator
Since the object is to rotate the load, and speed adjustment is necessary, allow an extra margin of 10 times or more in the effective torque.

* Actuator effective torque $\leq S \cdot T_a$
(S is 10 times or more)

Accelerating torque calculation



$T_a = I \cdot \dot{\omega}$ (N·m)
I : Moment of inertia
Refer to page 11.
 $\dot{\omega}$: Angular acceleration
 $\dot{\omega} = \frac{2\theta}{t^2}$ (rad/s²)
 θ : Rotation angle (rad)
t : Rotation time (S)

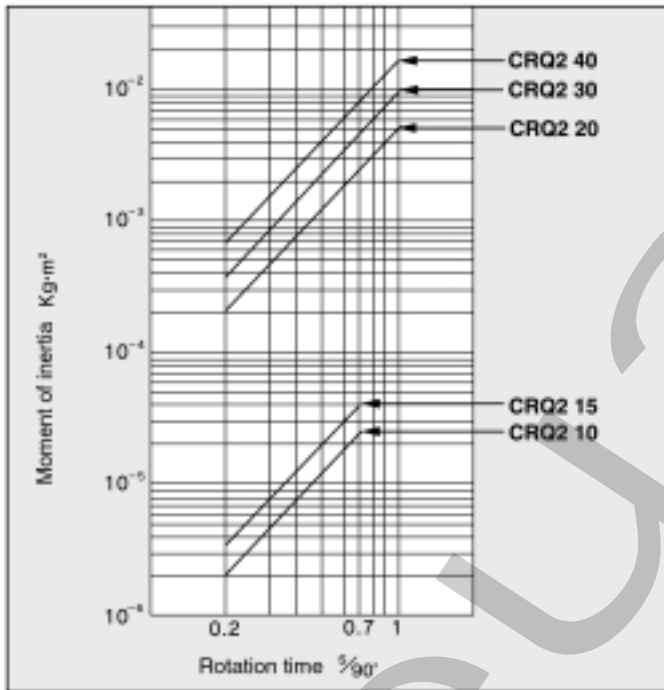
Step

2

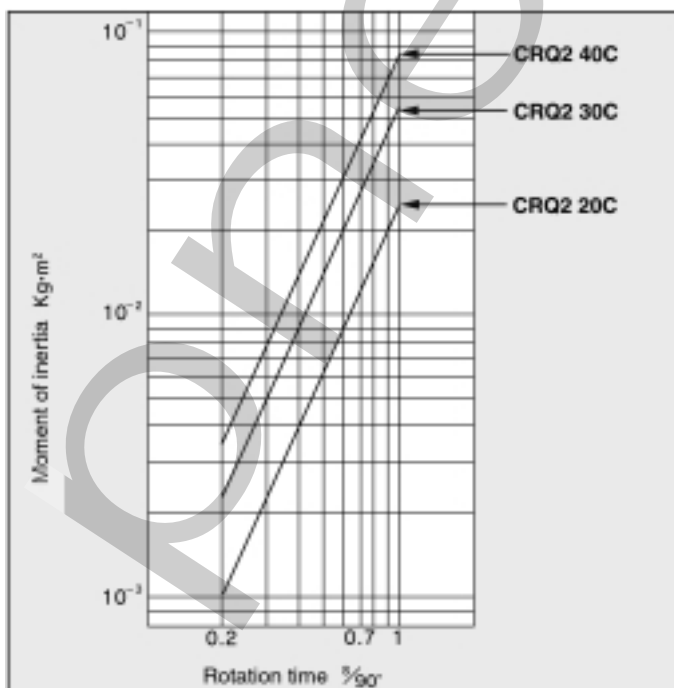
Consider the impact at the end of the rotation.

1. When an external stopper (shock absorber) is provided to absorb the impact, be sure to use one which has sufficient absorption capacity.
2. When relying on the actuator's internal cushion without using a stopper, the model selection graphs consider the absorption capacity of the actuator's internal cushion, making it possible to select a model from the rotation time within the speed adjustment range and the moment of inertia of the work piece.
 - 1) Rubber bumper ... Kinetic energy is absorbed by placing an elastic body (rubber) at the end of the rotation.
 - 2) Air cushion The exhaust air is compressed shortly before the end of the rotation, and the load's kinetic energy is absorbed by its repulsive force.

Without cushion



With cushion

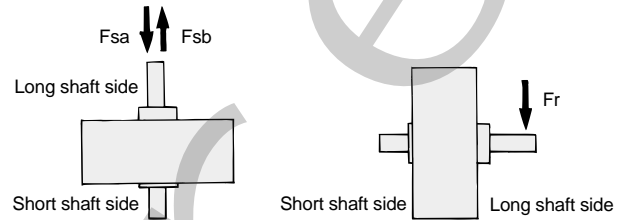


Step

3

Consider the allowable shaft load.

A load can be applied in the axial direction up to the values shown in the table below provided that a dynamic load is not generated. However, applications which apply a load directly to the shaft should be avoided whenever possible.

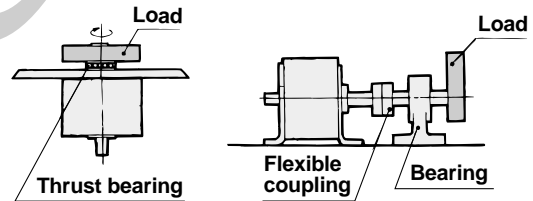


Rack-and-pinion type (double rack)

Unit: N

Size	Load direction		
	F _{sa}	F _{sb}	Fr
10	15.7	7.8	14.7
15	19.6	9.8	19.6
20	49	29.4	49
30	98	49	78
40	108	59	98

A load up to the allowable radial/thrust load can be applied provided that a dynamic load is not generated. However, applications which apply a load directly to the shaft should be avoided whenever possible. In order to further improve the operating conditions, a method such as that shown in the drawing below is recommended so that a direct load is not applied to the shaft.



Step

4

Find the air consumption of the actuator.

Find the air consumption necessary to calculate the running cost of the air supply. Refer to air consumption on page 18.

Rotary Actuator Technical Data 1 and 2 Effective Torque/Moment of Inertia

Effective Torque

Effective torque values are typical values and are not guaranteed.
Use them as guide values in actual applications.

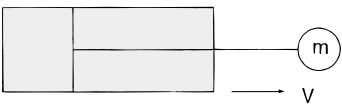
Unit: N·m

Size	Operating pressure (MPa)										
	0.10	0.15	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	1.00
10	—	0.09	0.12	0.18	0.24	0.30	0.36	0.42	—	—	—
15	—	0.22	0.30	0.45	0.60	0.75	0.90	1.04	—	—	—
20	0.37	0.55	0.73	1.10	1.47	1.84	2.20	2.57	2.93	3.29	3.66
30	0.62	0.94	1.25	1.87	2.49	3.11	3.74	4.37	4.99	5.60	6.24
40	1.06	1.59	2.11	3.18	4.24	5.30	6.36	7.43	8.48	9.54	10.6

Moment of Inertia

When an object (load) is moved by the actuator, inertial force (kinetic energy) is created in the object. Conversely, in order to stop the moving object, it is necessary to absorb the object's kinetic energy with a stopper or shock absorber, etc. When the load moves in a straight line (air cylinder) or turns (rotary actuator), the kinetic energies can be calculated with the formulas shown in Figures 1 and 2 respectively.

Air cylinder

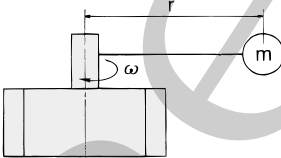


$$E = \frac{1}{2} \cdot m \cdot V^2 \dots \dots \dots \text{Formula (1)}$$

E : Kinetic energy
m : Load mass
V : Speed

Figure 1. Linear motion

Rotary actuator



$$E = \frac{1}{2} \cdot I \cdot \omega^2 = \frac{1}{2} \cdot m \cdot r^2 \cdot \omega^2 \dots \dots \text{Formula (2)}$$

E : Kinetic Energy
I : Moment of Inertia (=m·r²)
ω : Speed

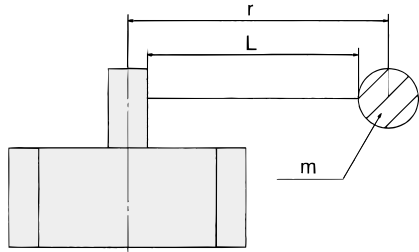
Figure 2. Turning motion

In the case of linear motion, if the speed "V" from Formula (1) is constant, the kinetic energy "E" is readily determined by the mass "m". However, in the case of turning motion it is clear from Formula (2) that the kinetic energy "E" varies in proportion to the square of the turning radius "r", even if the angular speed "ω" and mass "m" are constant. Thus, even if the mass is small, when "r" is large the resulting moment of inertia (I= m·r²) is large, and since the kinetic energy "E" also becomes large, this may lead to damage of the shaft, etc. When a load is moved in this way by a rotary actuator, it is particularly necessary to exercise caution regarding the moment of inertia (= m·r²) of the load.

A Moment of Inertia

The moment of inertia indicates the difficulty of turning an object, or conversely, the difficulty of stopping an object which is turning. Since there is a limit to the kinetic energy allowed in a rotary actuator, the limit value of the rotation time can be found by finding the moment of inertia. How to find the moment of inertia is explained below.

The basic formula for moment of inertia is shown below.



$$I = m \cdot r^2 \quad m : \text{Mass (kg)}$$

(However, the weight of the L section is ignored)

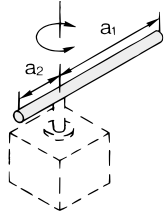
This indicates the moment of inertia with respect to the rotation axis of a mass "m" which is a distance "r" from the rotational axis. The formula for finding the moment of inertia differs depending on the shape of the object. A reference table of formulas for calculating the moment of inertia is shown on page 15.

Concrete examples of how to calculate the moment of inertia are shown on the following pages.

B **Moment of Inertia Formula Table (Calculation of Moment of Inertia) I: Moment of Inertia kg m² m: Load mass kg**

1. Thin shaft

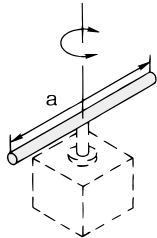
Position of rotational axis: Perpendicular to the shaft through one end



$$I = m_1 \cdot \frac{a_1^2}{3} + m_2 \cdot \frac{a_2^2}{3}$$

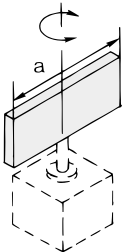
2. Thin shaft

Position of rotational axis: Through the shaft's center of gravity



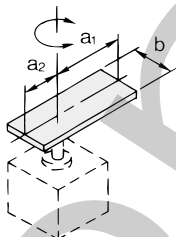
$$I = m \cdot \frac{a^2}{12}$$

3. Thin rectangular plate (rectangular parallelepiped) Position of rotational axis: Through the plate's center of gravity



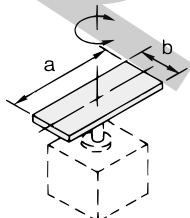
$$I = m \cdot \frac{a^2}{12}$$

4. Thin rectangular plate (rectangular parallelepiped) Position of rotational axis: Perpendicular to the shaft through one end (also the same in case of a thicker plate)



$$I = m_1 \cdot \frac{4a_1^2 + b^2}{12} + m_2 \cdot \frac{4a_2^2 + b^2}{12}$$

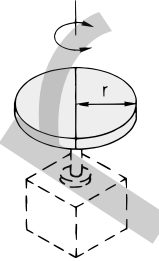
5. Thin rectangular plate (rectangular parallelepiped) Position of rotational axis: Through the center of gravity and perpendicular to the plate (also the same in case of a thicker plate)



$$I = m \cdot \frac{a^2 + b^2}{12}$$

6. Column (including thin round plate)

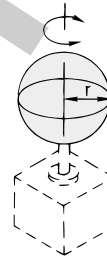
Position of rotational axis: Central axis



$$I = m \cdot \frac{r^2}{2}$$

7. Solid sphere

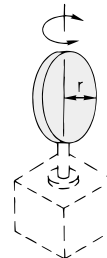
Position of rotational axis: Diameter



$$I = m \cdot \frac{2r^2}{5}$$

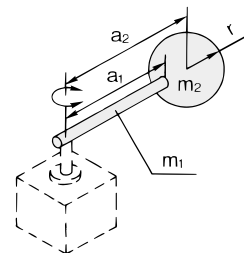
8. Thin round plate

Position of rotational axis: Diameter



$$I = m \cdot \frac{r^2}{4}$$

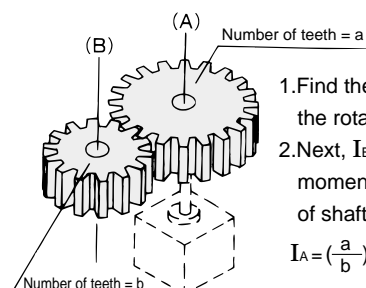
9. Load at end of lever



$$I = m_1 \cdot \frac{a_1^2}{3} + m_2 \cdot a_2^2 + K$$

(Example) When shape of m_2 is a sphere refer to 7 and $K = m_2 \cdot \frac{2r^2}{5}$

10. Gear transmission

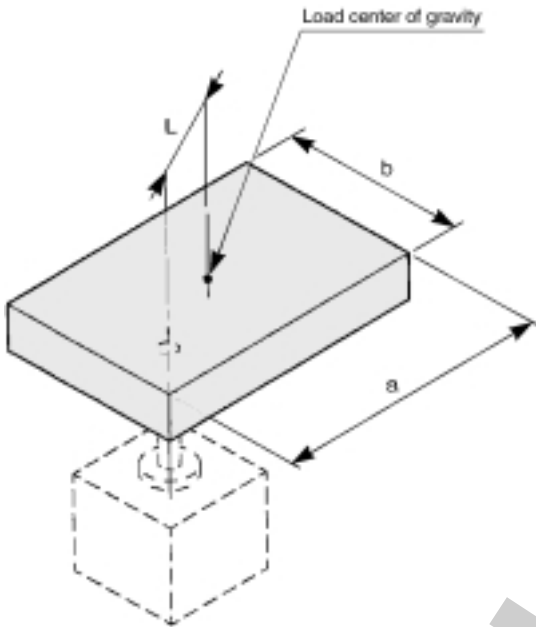


1. Find the moment of inertia I_B for the rotation of shaft (B).
 2. Next, I_B is entered to find I_A the moment of inertia for the rotation of shaft (A) as
- $$I_A = \left(\frac{a}{b}\right)^2 \cdot I_B$$

Technical Data/Moment of Inertia

C Moment of Inertia Calculation Examples

1 Rotational Axis at Random Point in Load



Example) When load is a rectangular shape as in technical data 5
Find I_1 with the load center of gravity at the tentative rotational axis.

$$I_1 = m \cdot \frac{a^2 + b^2}{12} \quad \text{kg} \cdot \text{m}^2$$

Find the moment of inertia I_2 for rotation around the actual rotational axis with the mass of the load concentrated at the load's center of gravity.

$$I_2 = m \cdot L^2 \quad \text{kg} \cdot \text{m}^2$$

Find the actual moment of inertia I .

$$I = I_1 + I_2 \quad \text{kg} \cdot \text{m}^2$$

(m : Load mass kg
 L : Distance from the rotational axis to the load center of gravity m)

Calculation example

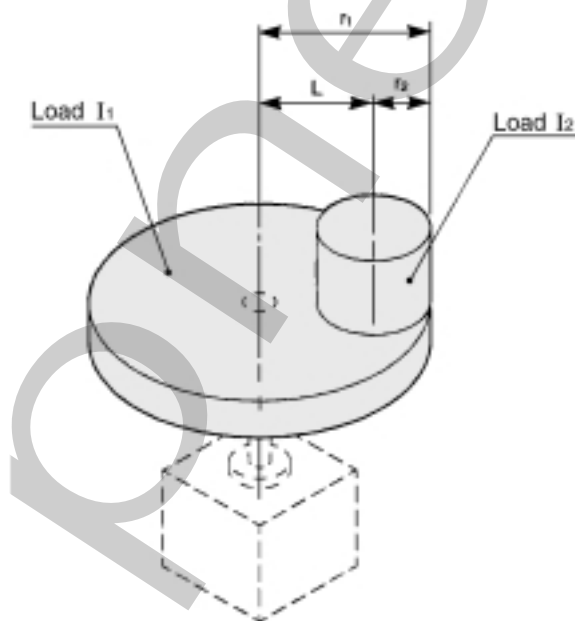
When $a = 0.2\text{m}$, $b = 0.1\text{m}$, $L = 0.05\text{m}$, $m = 1.5\text{kg}$

$$I_1 = 1.5 \times \frac{0.2^2 + 0.1^2}{12} = 6.25 \times 10^{-3} \quad \text{kg} \cdot \text{m}^2$$

$$I_2 = 1.5 \times 0.05^2 = 3.75 \times 10^{-3} \quad \text{kg} \cdot \text{m}^2$$

$$I = (6.25 + 3.75) \times 10^{-3} = 0.01 \quad \text{kg} \cdot \text{m}^2$$

2 Load Divided into Multiple Parts



Example) When load is divided into two columns such as shown in technical data 6

- { The center of gravity of load I_1 coincides with the rotational axis
 - { The center of gravity of load I_2 is different than the rotational axis
- Find the inertial moment of load I_1

$$I_1 = m_1 \cdot \frac{r_1^2}{2} \quad \text{kg} \cdot \text{m}^2$$

Find the moment of inertia of load I_2

$$I_2 = m_2 \cdot \frac{r_1^2}{2} + m_2 \cdot L^2 \quad \text{kg} \cdot \text{m}^2$$

Find the actual moment of inertia I .

$$I = I_1 + I_2 \quad \text{kg} \cdot \text{m}^2$$

(m_1, m_2 : Mass of loads I_1 and I_2 kg
 r_1, r_2 : Diameters of loads I_1 and I_2 m
 L : Distance from the rotational axis to load I_2 center of gravity m)

Calculation example

When $m_1 = 2.5\text{kg}$, $m_2 = 0.5\text{kg}$, $r_1 = 0.1\text{m}$, $r_2 = 0.02\text{m}$, $L = 0.08\text{m}$

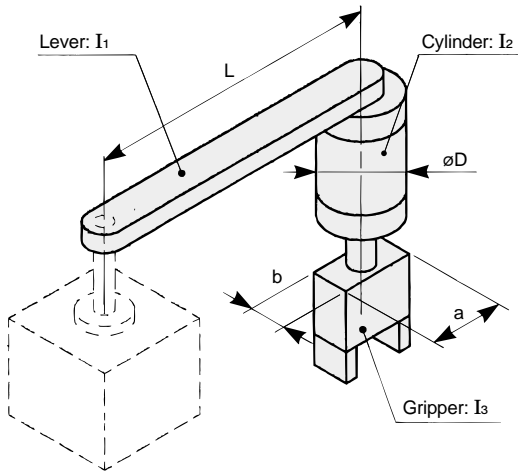
$$I_1 = 2.5 \times \frac{0.1^2}{2} = 1.25 \times 10^{-2} \quad \text{kg} \cdot \text{m}^2$$

$$I_2 = 0.5 \times \frac{0.02^2}{2} + 0.5 \times 0.08^2 = 0.33 \times 10^{-2} \quad \text{kg} \cdot \text{m}^2$$

$$I = (1.25 + 0.33) \times 10^{-2} = 1.58 \times 10^{-2} \quad \text{kg} \cdot \text{m}^2$$

Specific Application Example

3 Lever attached to shaft with cylinder and gripper mounted at end of lever



Example) Find the lever's moment of inertia.

$$I_1 = m_1 \cdot \frac{L^2}{3} \quad \text{kg}\cdot\text{m}^2$$

Find the cylinder's moment of inertia.

$$I_2 = m_2 \cdot \frac{D^2}{8} + m_2 \cdot L^2 \quad \text{kg}\cdot\text{m}^2$$

Find the gripper's moment of inertia.

$$I_3 = m_3 \cdot \frac{a^2+b^2}{12} + m_3 \cdot L^2 \quad \text{kg}\cdot\text{m}^2$$

Find the actual moment of inertia.

$$I = I_1 + I_2 + I_3 \quad \text{kg}\cdot\text{m}^2$$

(m_1 : Lever mass kg
 m_2 : Cylinder mass kg
 m_3 : Gripper mass kg)

Calculation example

When $L = 0.2\text{m}$, $\varnothing D = 0.06\text{m}$, $a = 0.06\text{m}$, $b = 0.03\text{m}$, $m_1 = 0.5\text{kg}$, $m_2 = 0.4\text{kg}$, $m_3 = 0.2\text{kg}$

$$I_1 = 0.5 \times \frac{0.2^2}{3} = 0.67 \times 10^{-2} \quad \text{kg}\cdot\text{m}^2$$

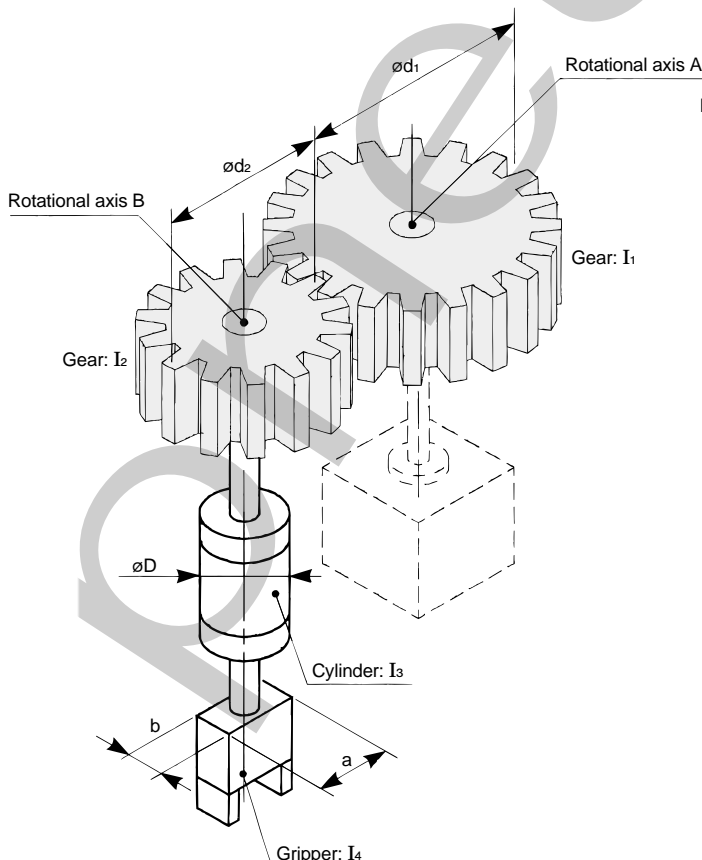
$$I_2 = 0.4 \times \frac{0.06^2}{8} + 0.4 \times 0.2^2 = 1.62 \times 10^{-2} \quad \text{kg}\cdot\text{m}^2$$

$$I_3 = 0.2 \times \frac{0.06^2 + 0.03^2}{12} + 0.2 \times 0.2^2 = 0.81 \times 10^{-2} \quad \text{kg}\cdot\text{m}^2$$

$$I = (0.67 + 1.62 + 0.81) \times 10^{-2} = 3.1 \times 10^{-2} \quad \text{kg}\cdot\text{m}^2$$

Specific Application Example

4 Load is rotated via gears



Example) Find the moment of inertial I_1 for rotation around shaft A.

$$I_1 = m_1 \cdot \frac{d_1^2}{8} \quad \text{kg}\cdot\text{m}^2$$

Find the moments of inertial I_2, I_3, I_4 for rotation around shaft B.

$$I_2 = m_2 \cdot \frac{d_2^2}{8} \quad \text{kg}\cdot\text{m}^2 \quad I_3 = m_3 \cdot \frac{D^2}{8} \quad \text{kg}\cdot\text{m}^2$$

$$I_4 = m_4 \cdot \frac{a^2 + b^2}{12} \quad \text{kg}\cdot\text{m}^2 \quad I_B = I_2 + I_3 + I_4 \quad \text{kg}\cdot\text{m}^2$$

Substitute the moment of inertia I_B for rotation around shaft B with the moment of inertia I_A for rotation around shaft A.

$$I_A = (A/B)^2 \cdot I_B \quad [A/B: \text{Gear tooth ratio}]$$

Find the actual moment of inertia.

$$I = I_1 + I_A \quad \text{kg}\cdot\text{m}^2$$

(m_1 to m_4 : Mass of I_1 to I_4 kg)

Calculation example

When $d_1 = 0.1\text{m}$, $d_2 = 0.05\text{m}$, $D = 0.04\text{m}$, $a = 0.04\text{m}$, $b = 0.02\text{m}$
 $m_1 = 1\text{kg}$, $m_2 = 0.4\text{kg}$, $m_3 = 0.5\text{kg}$, $m_4 = 0.2\text{kg}$, Gear tooth ratio = 2

$$I_1 = 1 \times \frac{0.1^2}{8} = 1.25 \times 10^{-3} \quad \text{kg}\cdot\text{m}^2 \quad I_4 = 0.2 \times \frac{0.04^2 + 0.02^2}{12} = 0.03 \times 10^{-3} \quad \text{kg}\cdot\text{m}^2$$

$$I_2 = 0.4 \times \frac{0.05^2}{8} = 0.13 \times 10^{-3} \quad \text{kg}\cdot\text{m}^2 \quad I_B = (0.13 + 0.1 + 0.03) \times 10^{-3} = 0.26 \times 10^{-3} \quad \text{kg}\cdot\text{m}^2$$

$$I_3 = 0.5 \times \frac{0.04^2}{8} = 0.1 \times 10^{-3} \quad \text{kg}\cdot\text{m}^2 \quad I_A = 2^2 \times 0.26 \times 10^{-3} = 1.04 \times 10^{-3} \quad \text{kg}\cdot\text{m}^2$$

$$I = (1.04 + 1.25) \times 10^{-3} = 2.29 \times 10^{-3} \quad \text{kg}\cdot\text{m}^2$$

Rotary Actuator Technical Data 3

Air Consumption

Air consumption is the volume of air which is expended by the rotary actuator's reciprocal operation inside the actuator and in the piping between the actuator and the switching valve, etc. This is necessary for selection of a compressor and for calculation of its running cost.

* The air consumption (Q_{CR}) required for one reciprocation of the rotary actuator alone is shown in the table below, and can be used to simplify the calculation.

Formulas

Q_{CR}: Since the internal volume is different when the A/B ports are pressurized in vane type sizes 10, 15, 20 and 30, use formula (1). Use formula (2) for vane type sizes 50, 80, 100 and the rack-and-pinion type.

$$Q_{CR} = V \times \left(\frac{P + 0.1013}{0.1013} \right) \times 10^{-3} \dots \dots \dots \text{Formula (1)}$$

$$Q_{CR} = 2V \times \left(\frac{P + 0.1013}{0.1013} \right) \times 10^{-3} \dots \dots \dots \text{Formula (2)}$$

$$Q_{CP} = 2 \times a \times l \times \frac{P}{0.1013} \times 10^{-6} \dots \dots \dots (3)$$

$$Q_C = Q_{CR} + Q_{CP} \dots \dots \dots (4)$$

- Q_{CR} = Air consumption of rotary actuator [/(ANR)]
- Q_{CP} = Air consumption of tubing or piping [/(ANR)]
- V = Internal volume of rotary actuator [cm³]
- P = Operating pressure [MPa]
- l = Length of piping [mm]
- a = Internal cross section of piping [mm²]
- Q_C = Air consumption required for one reciprocation of rotary actuator [/(ANR)]

When selecting a compressor, it is necessary to choose one which has sufficient reserve for the total air consumption of pneumatic actuators downstream. This is affected by factors such as leakage in piping, consumption by drain valves and pilot valves, etc., and reduction of air volume due to drops in temperature.

Formula

$$Q_{C2} = Q_C \times n \times \text{Number of actuators} \times \text{Reserve factor}$$

Q_{C2} = Compressor discharge flow rate

n = Actuator reciprocations per minute

Internal cross section of tubing and steel piping

Nominal size	O.D. (mm)	I.D. (mm)	Internal cross section a (mm ²)
T□ 0425	4	2.5	4.9
T□ 0604	6	4	12.6
TU 0805	8	5	19.6
T□ 0806	8	6	28.3
1/8B	—	6.5	33.2
T□ 1075	10	7.5	44.2
TU 1208	12	8	50.3
T□ 1209	12	9	63.6
1/4B	—	9.2	66.5
TS 1612	16	12	113
3/8B	—	12.7	127
T□ 1613	16	13	133
1/2B	—	16.1	204
3/4B	—	21.6	366
1B	—	27.6	598

Rack-and-pinion type: Series CRQ2

Air consumption of rotary actuator: Q_{CR} / (ANR)

Size	Rotation angle (°)	Internal volume V (cm ³)	Operating pressure (MPa)										
			0.1	0.15	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0
10	90	1.2	—	0.0060	0.0071	0.0095	0.0119	0.0142	0.0166	0.0190	—	—	—
	180	2.2	—	0.0109	0.0131	0.0174	0.0218	0.0261	0.0305	0.0348	—	—	—
15	90	2.9	—	0.0144	0.0173	0.0230	0.0287	0.0344	0.0402	0.0459	—	—	—
	180	5.5	—	0.0273	0.0327	0.0436	0.0544	0.0653	0.0762	0.0870	—	—	—
20	90	7.8	0.0310	0.0387	0.0464	0.0618	0.0772	0.0926	0.108	0.123	0.139	0.154	0.170
	180	13.4	0.0533	0.0665	0.0797	0.106	0.133	0.159	0.186	0.212	0.233	0.265	0.291
30	90	11.8	0.0469	0.0585	0.0702	0.0935	0.117	0.140	0.163	0.187	0.210	0.233	0.257
	180	22.7	0.0902	0.113	0.135	0.180	0.225	0.269	0.314	0.359	0.404	0.449	0.494
40	90	20	0.0795	0.099	0.119	0.158	0.198	0.237	0.277	0.316	0.356	0.395	0.435
	180	38.5	0.153	0.191	0.229	0.305	0.381	0.457	0.533	0.609	0.685	0.761	0.837